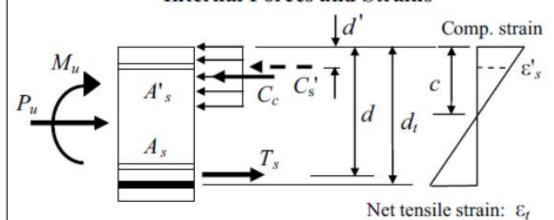
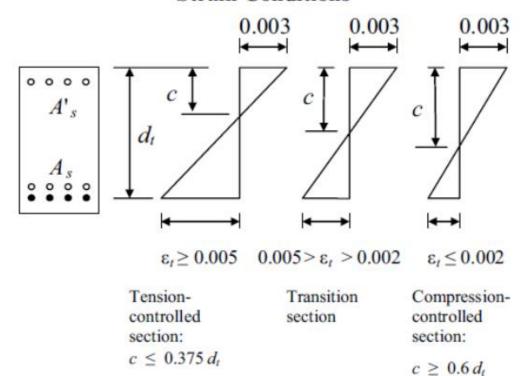
Beam Design Provisions- Singly and Doubly

UNIFIED DESIGN PROVISIONS

Internal Forces and Strains



Strain Conditions



For all beams

Net tensile strain: $a = \beta_1 c$

$$\varepsilon_t = \frac{0.003(d_t - c)}{c} = \frac{0.003(\beta_1 d_t - a)}{a}$$

Design moment strength: ϕM_n

where:
$$\phi = 0.9 \ [\epsilon_t \ge 0.005]$$

 $\phi = 0.48 + 83\epsilon_t \ [0.004 \le \epsilon_t < 0.005]$

Reinforcement limits:

$$A_{S, max} \quad \varepsilon_t = 0.004 \ @M_n$$

$$A_{S, min} = \operatorname{larger} \left\{ \frac{3\sqrt{f_c'b_w'}}{f_y} \text{ or } \frac{200b_w'd}{f_y} \right\}$$

 $A_{s,min}$ limits need not be applied if A_s (provided) $\geq 1.33 A_s$ (required)

Singly-reinforced beams

$$A_{s,max} = \frac{0.85 f_c ' \beta_1 b}{f_y} \left(\frac{3d_t}{7} \right)$$

$$A_s f_v$$

$$a = \frac{A_s f_y}{0.85 f_c' b}$$

$$M_n = 0.85 f_c' a b (d - \frac{a}{2}) = A_s f_y (d - \frac{a}{2})$$

Doubly-reinforced beams

Compression steel yields if:

$$A_s - A_s' \ge \frac{0.85\beta_1 f_c'd'b}{f_y} \left(\frac{87,000}{87,000 - f_y} \right)$$

If compression steel yields:

$$A_{s,max} = \frac{0.85 f_c' \beta_1 b}{f_y} \left(\frac{3 d_t}{7} \right) + A_s'$$

$$a = \frac{(A_s - A_s') f_y}{0.85 f_c' b}$$

$$M_n = f_y \left[\left(A_s - A_s' \right) \left(d - \frac{a}{2} \right) + A_s' (d - d') \right]$$

If compression steel does not yield (two steps):

1. Solve for c:

$$c^{2} + \left(\frac{(87,000 - 0.85 f_{c}') A_{s}' - A_{s} f_{y}}{0.85 f_{c}' \beta_{1} b}\right) c$$
$$-\frac{87,000 A_{s}' d'}{0.85 f_{c}' \beta_{1} b} = 0$$

2. Compute M_n :

$$M_n = 0.85 b c \beta_1 f_c' \left(d - \frac{\beta_1 c}{2} \right)$$
$$+ A_s' \left(\frac{c - d'}{c} \right) (d - d') 87,000$$